
Investigation of Peanut Shell as Alternative Sound Absorbing Material

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Abstract: Use of natural material for development of sound absorbers received considerable significance since in past few years. Natural materials are preferred due to their ease of availability, low environmental impact, distinctive internal structure and reusability. One such natural material Peanut shell is made up of natural cellulose fibers and has good internal pores which can be utilized for sound absorption application. In the current study samples of Peanut shell specimens were made of 100mm diameter having different material to binder weight ratios. The test specimens were made with thickness 10mm, 15mm, 20mm, 25mm, 30mm, 35mm and 40mm respectively. Normal incidence sound absorption coefficient for the specimens is measured using ASTM E1050-98 (Standard Test Method for Impedance and Absorption of Acoustical Materials Using a Tube, Two Microphones, and a Digital Frequency Analysis System) and values of the normal incidence sound absorption are compared with values obtained using Delany and Bazley Model. It was observed that Peanut shell test specimen with material to binder weight ratio 70:30 gives optimum average sound absorption for frequency range between 250Hz to 4500Hz. The current paper concludes that Peanut shell can prove to be good alternative natural material over existing conventional sound absorbing materials for application in field of sound absorption.

Keywords: Acoustics, Impedance Tube, Noise, Peanut Shell, Sound Absorption Coefficient, Natural Fibers

1. Introduction

Need for creating more comfortable environment in specific areas like schools, offices, hospitals, industries, malls, theaters and study centers is mandatory. Many engineering and architectural techniques are adopted to solve the noise related problems to environmental conditions at such places. Noise is the greatest concern which is required to be controlled at minimal expenses. At present synthetic sound absorbing materials like glass wool, rock wool, shoddy and polyurethane foams are used for controlling the noise level at these places. Use of synthetic materials has its limitations as they are expensive, non-degradable and non-recyclable. These limitations lead to conduct more research for alternative solution on the synthetic materials.

2. Literature Survey

Hasina Mamtaz et al. [1] developed natural sound absorber from the composition of fibrous and granular materials. Their

effort in manufacturing of composite sound absorbing materials with coconut coir fiber and rice husk had additional benefits like cost effective and efficient performance. The sound absorption coefficient is measured by using a set of two impedance tube as per ASTM E1050-98 standard. And the results obtained were compared with the existing synthetic materials especially at low frequencies. Zhengqing Lou et al. [2] in their work on multilayer sound absorbers having various layers of 3D printed micro perforated polymeric panel and non-woven recycled cotton backing gave them efficient way of obtaining better results at higher frequency sound absorption. C. Arenas et al. [3] in their efforts on use of alternate methodology for measurement of sound absorption of composite materials manufactured using coal bottom ash formed by pulverized coal combustion. Acoustic behavior for materials with different thickness and multilayer composite products is predicted using the intrinsic properties like porosity and static airflow resistivity which were found using impedance tube. Results from the simulation software SIMAM and CARAM were compared with the values

obtained using the reverberation room method.

A. Farhad Forouharmajd et al. [4] in their efforts in investigation of normal incidence sound absorbing capacity of materials manufactured from polyurethane foam, polystyrene, polyvinylchloride (PVC), rubber, mineral wool carpet and glass samples. Wherein the specimen thickness 25mm is kept constant for all the test samples and it is found that mineral wool gives sound absorption of about 0.97 at frequency range between 500 Hz to 4500 Hz. Khai Hee Or et.al [5] believed that the oil palm empty fruit bunch fiber could prove to be sustainable option as alternative sound absorbing materials. They obtained the fibers by mechanical retting process and further prepared the samples having diameter 33 mm and different thickness. Samples are prepared by compression of fibers in aluminum mold at 100°C for 5 minutes. Test for sound absorption is performed on impedance tube using ISO 10534-2 standard for determination of sound absorption coefficient and impedance in impedance tubes by varying density, air gap and thickness of samples. It was observed that the absorption coefficient improves with increase in air gap and increase in density till a certain point beyond which later sound absorption decreases. B. Botterman et al. [6] discussed modeling and optimization of wood wool cemented boards to deliver more effective model for obtaining better accuracy in predicting sound absorption coefficients for wood wool cemented boards. They had compared three impedance model namely Attenborough model, Johnson- Champoux- Allard (JCA) model and Johnson- Champoux- Allard-Lafarge (JCAL) Model. The authors reported that JCA model gives better results as compared to other model as it takes five parameter into consideration namely porosity, flow resistivity, tortuosity, viscous and thermal characteristic lengths that largely influence the sound absorption. Manthan Sambu et al. [7] prepared sound absorber from non-woven aregna pinnata (ijuk) fiber and natural rubber. While making samples the ijuk was firstly soaked in alkaline then mixed with natural rubber later on heating and compression was performed. Paper reports samples made with combinations of 80:20, 70:30, 60:40 of above combination with a 50 mm fixed thickness and diameter of 100 mm. It was observed that use of natural rubber as binder improves the sound absorption coefficient. For frequency of 100 Hz Sound absorption average (SAA) was 0.9 for 80:20 composition which was found to be optimum. Hasina Mamtaz et al. [8] mentions the drawbacks of use of natural fiber without support of synthetic fibers. Paper reports composite sound absorbing materials made up of fibro granular material mixed with natural rubber and polymer fiber matrix. As the rubber granules have high porosity which further improves tortuosity and flow resistivity. It is observed that decrease in rubber grain size improves the sound absorption whereas alkaline treatment gives good low frequency sound absorption and increase in the air flow resistivity with improvement in overall performance. Ancuta-Elena

Tiuc et al. [9] introduced the use of textile waste for improving the sound absorption for polyurethane foam. Isocyanate polyol mixture gives polyurethane foam with blow agent as catalyst forms to produce rigid composite matrix with textile waste. It is observed that combination of 75% rigid polyurethane foam (RPF) and 25% textile waste gives SAA of 0.86 at 1000Hz which is seen as better among other combinations. Cinzia Burtti et al. [10] used recycled materials for building applications to achieve low cost production of panels. Paper reports use of recycled paper and other scrap materials as wool and nonwoven polyester fabric due to their good acoustic behavior. Samples with diameter of 29 mm and 100 mm were manufactured with different thickness. These samples were tested on two microphone impedance tube of standard ISO 10534-2. Both types of panels were applied on ceilings of lecture hall. It was observed that performance of recycled material panels meets the performance of conventional material panels. Daniela Bosnia et. al [11] had used recycled sheep wool as sound absorbing material as it has advantages like biodegradable and easy available. Test panels were made with area of 12 m² and 50 mm thickness and 130 kg.m⁻³ density. Specimens were tested for frequency range between 100Hz to 500Hz. It was found that sheep wool gives good absorption at low as well as high frequencies as compared to glass and rock wool having similar density. M. T. Fadzlitia et al. [12] made use of coir fiber material panels for application in sound absorption. Objective of work was to study the effect of varying percentage of perforated zinc plates covering the coir fiber panel in order to improve the acoustic performance. The perforated sheet with 6.92% and 19.23% perforation percentages were used with the panels. It was found the high perforation percentages increase the sound absorption. The peak value like 0.73 was achieved at frequency of 2000Hz. A. K. Elwaleed et al. [13] had approach for utilization of date palm fiber as sound absorbing material. Average diameter of fiber is around 0.408 mm with density of 919 Kg.m⁻³ respectively. Mold with two different diameter and range of sizes were used to prepare samples. Uncompressed sample size 30 mm is compressed to a thickness of 23 mm with compression ratio of 1.3, it was observed that the value of absorption coefficient increase with increase in flow resistivity. As the compression rate is increased to 2.3 the performance of the sample decreases. Tucheng Hung et al. [14] efforts on the use of blast furnace slag of calcium oxide and silicon dioxide for manufacturing of inorganic polymeric foam (IPF). Paper reports use of inorganic polymeric foam as sound absorbing materials. Foams were manufactured with densities 0.4, 0.6, 0.8 and 1.0g.cm⁻³ and were cut in size of 4 cm and 6 cm thickness respectively. It was observed that sound absorption increases as the density of specimen decreases from 1.0g.cm⁻³ to 0.4g.cm⁻³ regardless to frequency. Hai-fan Xiang et al. [15] suggested the use of kapok fiber for noise reduction applications. They had investigated

acoustical properties of the kapok fiber by use of modified Delany and Bazley model and normal absorption coefficient were found using the SW 466 Impedance tube (transfer function method). It was observed kapok fibers have good acoustical damping properties due to its hollow structure and hence can be used in noise reduction. Lamyaa Abd Al Rahman et al. [16] conducted study on the natural fiber for green acoustic absorbing materials. The two micro porous materials namely Date Palm Fiber (DPF) and Coconut Coir Fiber (CCF) are considered for the study. Samples with thickness range 10 mm-40 mm and density variation between 90-160 kg.m⁻³ were manufactured. Acoustical absorption coefficient values of DPF and CCF were compared with each other. It was observed that increase in the bulk density of natural fiber gives better performance in sound absorption. Sezgin Ersoy et al. [17] investigated the sound absorbing properties of industrial tea leaf fiber waste which is hygienic and ecofriendly in nature and can prove to be good alternative for manufacturing of acoustic absorbing materials. Samples form Woven Cotton Cloth (WCC), Propylene based nonwoven fiber (PNF) and Tea Leaf Fiber (TLF) were manufactured with thickness range of 10 mm, 20 mm, and 30 mm. Results were compared with each other and it was observed that TLF of 30 mm sample size gives SAA 0.75 for frequency range between 500-3500Hz.

It can be seen that there is extensive scope for use of natural materials for utilizing acoustic materials. Natural materials are preferred due to their ease of availability, low environmental impact, distinctive internal structure and reusability; they can prove to be good alternative over existing synthetic materials. Objective of this work is to investigate the sound absorbing potential of peanut shell waste (a natural material).

3. Test Specimen Preparation

Peanut also known as ground nut is a legume crop grown mainly for its edible seeds and cultivated in tropical or subtropical regions. Global annual production of shelled peanuts was 42 million tonnes in 2014 from which 6.6 million tonnes was produced in India. Large production generates large waste in the form of peanut shell. Peanut shell waste is commonly used in modern stock husbandry, biomass for house hold use or making of byproducts. Besides this peanut shell have low density, low thermal conductivity and porosity. To make the samples from the peanut shells, steel molds were prepared with internal diameter of 100mm with different thickness viz. 10mm, 15mm, 20mm, 25mm, 30 mm, 35mm and 40mm respectively. Steel mold were cut by using gas cutting machine as shown. Figure 1 shows the test Specimen of molds prepared with 100 mm diameter of various thickness.



Figure 1. Test Specimen Molds of 100mm diameter with various thickness range.

Figure 2 shows the flow chart of steps used for test specimen preparation from collection of peanut shell till sample preparation.

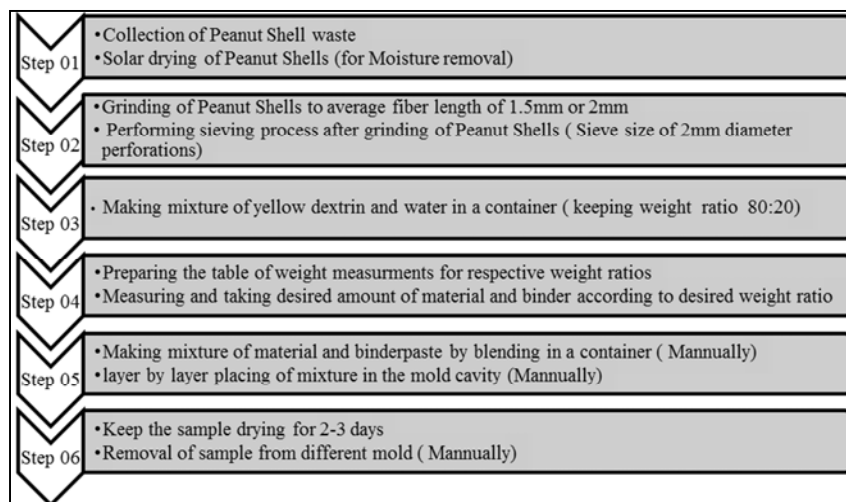


Figure 2. Steps for test specimen preparation process flow chart.

Molds are made in different thickness range with constant internal diameter of 100mm and outer diameter of 135mm respectively as shown in Figure 1. The sample preparation process has been briefed in the flow chart as shown in Figure 2. The process includes the use of blender, sieving equipment's

and clamps, plates, containers, brushes etc. Adhesive used in the sample preparation is yellow dextrin which is made of corn starch. It is referred to be natural binder for use in sample preparation. Yellow dextrin is available in the form of powder as industrial adhesive as shown in Figure 3.



Figure 3. Yellow dextrin powder.

Measurements of the material and binder were taken using electronic weight measuring machine having capacity to accurately measure from 1 gram. Samples made with different material to binder weight ratios (MBWR) 55:45, 60:40, 65:35, 70:30 and 75:25 as shown in Figure 4 to Figure 8.



Figure 6. Test Specimen with MBWR 65.35.



Figure 4. Test Specimen with material to binder weight ratio (MBWR) 55.45.



Figure 7. Test Specimen with MBWR 70.30.



Figure 5. Test Specimen with MBWR 60.40.



Figure 8. Test Specimen with MBWR 75.25.

These samples with different weight ratios have different bulk density for their respective thickness as shown in the Table 1.

Table 1. Bulk Densities values for test different Samples.

Weight Ratios		C1 (55:45)	C2 (60:40)	C3 (65:35)	C4 (70:30)	C5 (75:25)
Thickness in mm	Volume in mm ³	Density in kg/m ³	Density in kg/m ³	Density in kg/m ³	Density in kg/m ³	Density in kg/m ³
10	78539.81	611.2	636.6	585.7	611.2	471.1
15	117809.7	645.1	611.2	628.1	628.1	619.6
20	157079.6	604.8	541.1	547.5	598.4	515.7
25	196349.5	646.8	621.3	519.5	728.3	601
30	235619.5	619.6	636.6	539	679.1	700.3
35	274889.4	669.4	844	516.6	753	734.8
40	314159.3	684.4	830.8	592.1	774.8	735.3

4. Measurement of Sound Absorption Using Delany Bazley Model

Mathematical model applied for estimating the normal sound absorption values generally depends upon distinctive absorption mechanism and category of porosity of the material been evaluated. Delany and Bazley model (DB Model) is most widely used for predicting the normal sound absorption values especially for natural fibers and porous sound absorbing materials. It is a simple model and requires non acoustical parameter of air flow resistivity for predicting the sound absorption values. It considers the porous layers as bulk materials including the rigid frame media of sample. Air flow resistivity is sufficient to define the characteristic wave impedance (z_c) and propagation constant (k_c) also known as complex wave number, the model for finding the values of sound absorption (α) is given below:

Air Flow resistance of sample (R)

$$R = \frac{\Delta p}{Q} \quad (1)$$

Specific air flow resistance (R_s)

$$R_s = \frac{R}{A} \quad (2)$$

Air Flow resistivity of material (σ)

$$\sigma = \frac{R_s}{d} \quad (3)$$

$$z_c = \rho_0 c \left[1 + 0.078(\rho_0 f / \sigma)^{-0.623} \right] - j0.074(\rho_0 f / \sigma)^{-0.66} \quad (4)$$

$$k_c = \omega / c \left[1 + 0.0987(\rho_0 f / \sigma)^{-0.70} - j0.189(\rho_0 f / \sigma)^{-0.595} \right] \quad (5)$$

$$z_s = -jz_c \cot(k_c d) \quad (6)$$

$$r = (z_s - \rho_0 c) / (z_s + \rho_0 c) \quad (7)$$

$$\alpha = 1 - |r|^2 \quad (8)$$

Where,

ρ_0 = density of air (Kg.m^{-3})

c = Speed of sound at ambient conditions (m.s^{-1})

Q = Air flow rate ($\text{m}^3.\text{s}^{-1}$)

A = Area of sample specimen (m^2)

ΔP = Differential pressure (Pa.s.m^{-1})

f = Frequency (Hz)

ω = Angular Frequency (rpm)

σ = Static air flow resistivity (Pa.s.m^{-2})

d = Thickness of sample (m)

r = Sound pressure reflection coefficient

α = Sound absorption coefficient

5. Measurement of Sound Absorption Using Impedance Tube Test Setup

Impedance tube method (ASTM E1050-98) has more advantage when compared to other method because of its compact, low cost and speedy result generation features. In this method sound is created inside the impedance tube and made to incident on the acoustic material. From the reflected waves some of the characteristic of the acoustic materials can be calculated. Impedance tube method is well suitable for the small sample size where as in case of the reverberation chamber larger number of samples is used. Standing wave method and transfer function method are two commonly used method of impedance tube. It is the direct method which involves calculation of the standing wave ratio (SWR). In this method microphone is moved along the length of the impedance tube by means of the carrier assembly. This most common and simple method is used to calculate the absorption coefficient (α) of the materials only. Here the sound of particular frequency is produced by means signal generator.

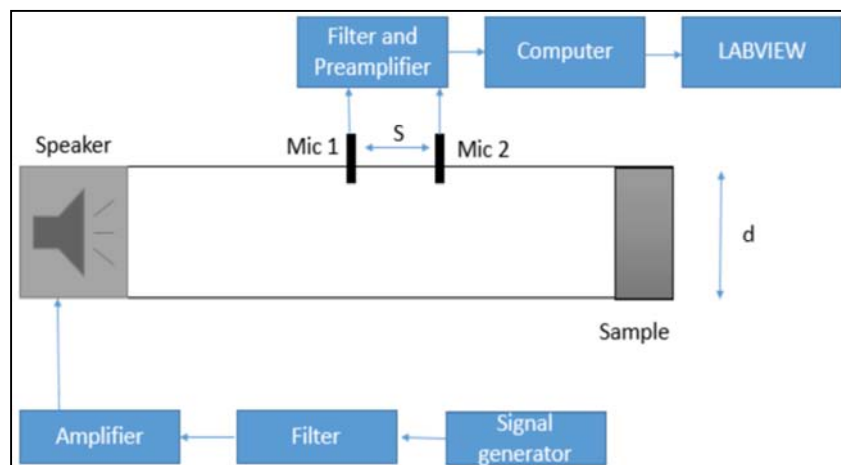


Figure 9. Schematic diagram of impedance tube test setup.

Figure 9 shows two microphone setup, loud speaker is kept at the one end of the impedance tube while the sample is kept

at the other end of the impedance tube. two microphones are kept at the particular interval inside the impedance tube. This

microphone converts the sound pressure inside the tube to respective voltage signal from that signal absorption coefficient can be calculated. Figure 10 shows Impedance tube test setup used for investigation of Sound absorption.



Figure 10. Impedance tube test setup.

Specifications of test setup:
 Measurement Standard: ASTM E1050-98
 Manufacturer: BSWA Technology Co., Ltd
 Model Number: SW 422 (63Hz~4500Hz)

6. Results and Discussion

Results obtained through experimentation are shown in the form of graphs for test specimens with different material to binder ratios as shown below:

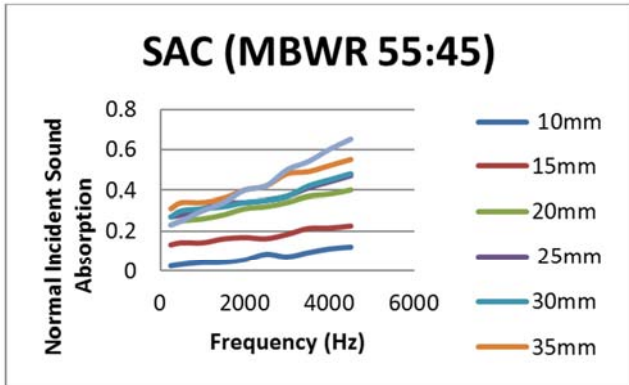


Figure 11. SAC for test specimen (MBWR 55.45).

From the Figure 11, it can be observed that sound absorption response curve for the test specimen with different thickness range is almost linear with respect to the frequency range of 250 Hz to 4500 Hz. The curves for the 25 mm, 30 mm, 35 mm and 45 mm thickness of test specimen intersect with each other at frequency range between 500 Hz to 1500 Hz due to the varying densities for respective specimens. The maximum sound absorption of 0.65 is obtained for the specimen having thickness 40 mm for the frequency of 4500 Hz. Similarly for the test specimen with thickness of 10 mm gives maximum sound absorption of 0.121 at the 4500Hz of frequency.

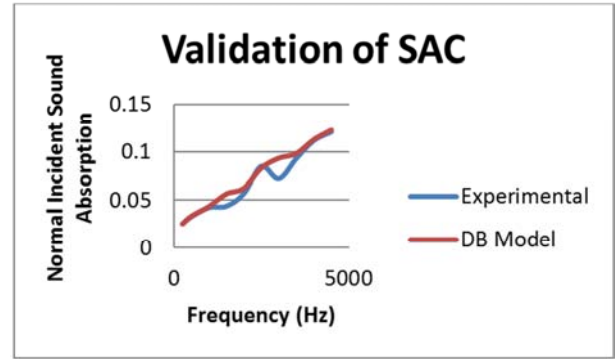


Figure 12. Comparison of results.

Validation of test results is done by comparison of the both experimental values with values obtained by the DB Model for the 10mm thickness test specimen with material to binder weight ratio 55:45 as shown in above the Figure 12.

Table 2. Comparison of SAC (10mm Specimen).

Frequency	Sound Absorption Coefficient	
	Experimental	DB Model
250	0.025	0.0252
500	0.0325	0.033
1000	0.0421	0.0432
1500	0.0435	0.0563
2000	0.0566	0.0622
2500	0.085	0.0832
3000	0.072	0.0935
3500	0.0932	0.0983
4000	0.112	0.113
4500	0.121	0.123
Avg. Value	0.06829	0.07309

Above table 2 describes comparison of experimental and model values of Sound absorption coefficient for the 10 mm thickness specimen with material to binder weight ratio of 55:45. It can be observed that average experimental sound absorption value 0.06829 for frequency range of 250Hz to 4500Hz. As the average value form the D B Model is 0.07309 for same frequency range. Percentage variation of the average experimental value from the average value obtained from the Delany & Bazley model is about 6.56%, Which is sufficient for verification of the experimental values with the values obtained from mathematical model.

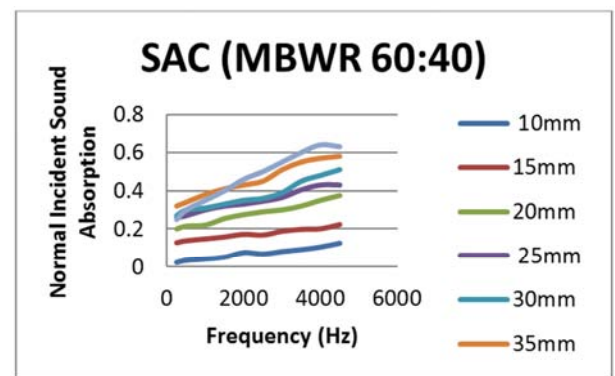


Figure 13. SAC for test specimen (MBWR 60.40).

From Figure 13 similar response curves are generated for the test specimen with range of thickness and material to binder weight ratio of 60:40. It can be observed that maximum sound absorption value for 40 mm thick specimen is 0.63 for frequency. SAC values for the frequency range between 250Hz to 2500Hz looks to be less than values compared with 35 mm thick specimen. This change occurs due to inherent porosity distribution throughout the specimen thickness.

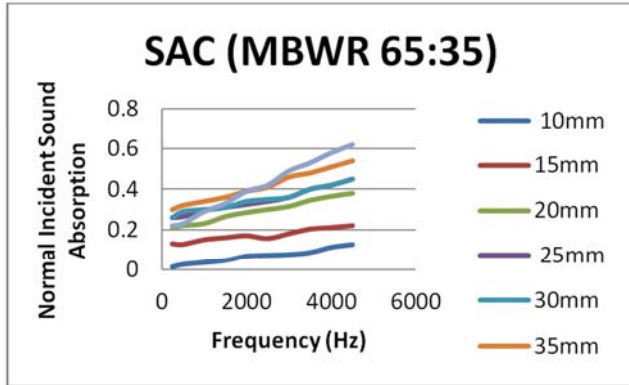


Figure 14. SAC for test specimen (MBWR 65.35).

Figure 14 shows the sound absorption response curves for the different specimens with material to binder weight ratio of 65:35. It is observed that maximum sound absorption value obtained for the 40mm thick sample is about 0.625 and for sample with thickness 30 mm is 0.545 for frequency of 4500Hz.

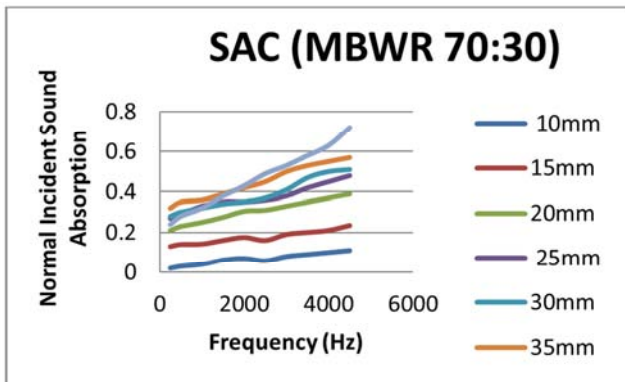


Figure 15. SAC for test specimen (MBWR 70.30).

Figure 15 shows the sound absorption response curves for the specimen with material to binder weight ratio of 70:30 for frequency range between 250Hz to 4500Hz. It is observed that specimen with thickness 40mm give maximum sound absorption of 0.72 at frequency of 4500Hz and the curves of different thickness specimens vary as per the change in their densities and porosity in the specimen thickness for the frequency range between 250Hz to 4500Hz.

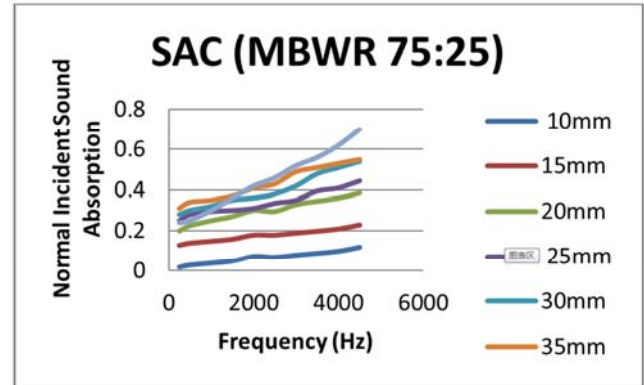


Figure 16. SAC for test specimen (MBWR 75.25).

Figure 16 shows the sound absorption response curves for the specimen with material to binder weight ratio of 75:25 for frequency range between 250Hz to 4500Hz. It is observed that specimen with thickness 40mm give maximum sound absorption of 0.70 at frequency of 4500Hz, but the values at lower frequencies is lower than values of specimen with 30mm thickness. This occurs due to curves of different thickness specimens vary as per the change in their densities and porosity in the specimen thickness for the frequency range between 250Hz to 4500Hz.

7. Conclusion

Observation of sound absorption average (SAA) for test specimen with different material to binder weight ratios and thickness varies as result of uncertainties due to non-uniform varying inherent physical properties such as porosity and flow resistivity. Peanut shell test specimen with material to binder weight ratio 70:30 gives optimum average sound absorption for frequency range between 250Hz to 4500Hz. Thus peanut shell could prove to be good alternative against existing synthetic sound absorbers.

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Conflict of Interest Statement

All the authors do not have any possible conflicts of interest.

Data Availability Statement

The experimental results data recorded and used in this. Research article are available from the corresponding author upon request.

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